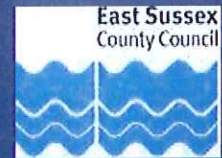


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**East Sussex County Council
Transport and Environment**

**Bexhill to Hastings Link Road
S12 Powdermill Stream Underbridge
Approval in Principle**

**Doc. Ref: B1297000-PH2/1600.06a/0012
Revision 0
August 2012**

Project: Bexhill to Hastings Link Road
Client: East Sussex County Council **Project No:** B1297000
Document title: Powdermill Stream UB AIP
Ref. No: B1297000-PH2/1600.06a/0012

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1. HIGHWAY DETAILS

1.1 Type of highway

Over: Bexhill to Hastings Link Road (BHLR) which is a single carriageway 2-lane rural all purpose road. 12.0m carriageway with 2.5m verge on the north side and 2.5m verge on the south side.

Under: N/A

1.2 Permitted traffic speed

Over: 60 mph

Under: N/A

1.3 Existing restrictions

None.

2. SITE DETAILS

2.1 Obstacles crossed

The bridge crosses Powdermill Stream, which flows from north to south, and an adjacent 3.0m wide country walk. The channel width, measured square between the tops of opposing banks is approximately 10.0m at its widest point below the footprint of the structure.

3. PROPOSED STRUCTURE

3.1 Description of structure

The structure is a single span underbridge carrying BHLR over Powdermill Stream. The deck consists of inverted prestressed concrete T-beams with concrete infill. The deck is integral with reinforced concrete abutment walls supported on a piled foundation. The reinforced concrete wingwalls are set generally parallel to the mainline alignment.

The parapet stringcourse will be cast in situ reinforced concrete.

The OS grid reference for the structure is 576055.7E, 110582.6N.

A ductile iron highway drainage pipe is attached behind the parapet system to the north side of the bridge.

Environmental barriers are attached to the outside of the parapet stringcourse along both edges of the structure. A separate Category 0 technical approval submission covers the environmental barriers generally although framing and fixings specific to this structure will be designed as part of the bridge structure submission.

3.2 Structural type

The structure is a single span integral bridge designed as a frame-type integral bridge in accordance with BA 42/96.

Wingwalls consist of a mixture of short sections cantilevering from the rear of the abutment and free-standing cantilever walls.

3.3 Foundation type

Reinforced CFA concrete piled foundation.

3.4 Span arrangements

Clear square span..... 14.3 m Skew angle 7 degrees

Clear skew span 14.4 m

3.5 Articulation arrangements

The structure is an integral bridge which does not require deck articulation or movement joints. BD33/94 Type 2 (Asphaltic plug) joints are proposed at the approach embankment/deck interfaces.

Thermal movement of the bridge deck is resisted by passive earth pressure behind the abutment wall and rotational stiffness of the end supports.

3.6 Types of road restraint systems

The proposed road restraint system requirement has been confirmed by a RRRAP assessment. A metal N2/W4 vehicle parapet 1000mm high with mesh infill will be provided to comply with the requirements of TD19/06.

An environmental (noise) barrier is fixed behind the parapet system on both sides of the bridge.

3.7 Proposed arrangements for maintenance and inspection

3.7.1 Traffic management

Close inspection or maintenance of the deck soffit over the waterway and the outer faces of the environmental barrier will require an underbridge unit and hence a single lane closure of the link road will be necessary.

3.7.2 Access

Over the waterway, the deck soffit can be accessed by underbridge unit from the carriageway above (with removal of environmental barrier). Alternatively, a MEWP positioned on the 1066 Path adjacent to the west abutment could be used.

A minimum 3.0m wide country walkway is to be provided in front of the west abutment wall. A minimum 2.3m clear headroom will be provided from the country walkway level to the underside of the precast beams. A minimum 2.0 wide clearance to top of bank will be provided in front of the east abutment wall.

Inspection and maintenance of the remaining deck soffit, abutments and wing walls can be carried out from ground level using a platform or ladder to reach upper levels.

Foundations will not be visible or accessible for inspection.

3.8.1 Materials and finishes

Concrete	Element	Limiting Exposure Class	
C48/60	Prestressed T beams	XD1	
C40/50	Infill deck slab	Top	XC3
		Cantilever soffit	XD3
		Parapet plinths	XD3
C32/40	Abutment, exposed face below deck	XD1	
	Abutment, wingwalls exposed side faces	XD3	

	Abutment, wingwalls buried	DC-1
C32/40	CFA Piles	DC-3z. Note A
Note A	ACEC class is AC-3z in natural ground therefore Design Chemical Class for pile design will be DC-3z. Refer to Geotechnical Summary Sheet for detail.	
Reinforcement	All reinforcement to be grade 500B or 500C deformed bars to BS 4449:2005	
Parapets	Painted (HA Type IV), galvanised steel.	
Backfill to abutments and retaining walls	Fill material to structures to be Class 6N or 6P in accordance with DoT Specification for Highway Works.	
Concrete Finishes		
Deck soffit ie PC beam soffits	F5	
Surfaces to receive waterproofing	U4	
Top of parapet plinth	U3	
Sides of parapet plinth	F3	
Abutment	F2	
Wingwalls	F6 (grooved patterned profile finish)	
Buried formed surfaces	F1	
Buried unformed surfaces	U1	

Protection

The top deck surface will be protected with a proprietary spray applied bridge deck waterproofing system to SHW CI 2003.

All accessible concrete surfaces greater than 150mm below finished ground level to receive waterproofing to below ground concrete surfaces in accordance with the SHW CI 2004.

3.8.2 Sustainability issues

Conventional construction materials are proposed, therefore, no significant sustainability issues are foreseen.

3.9 Risks and hazards considered

Standard construction methods are anticipated with normally associated risks and hazards. A design hazard log and risk assessment process is active for the scheme.

3.10 Estimated cost of proposed structure together with other structural forms considered and the reasons for their rejection including comparative whole-life costs with dates of estimates.

The relative advantages, disadvantages and costs of various structural forms are discussed and appraised in Owen Williams reports No. 262701/012 'BHLR Structures Options Report'.

3.11 Proposed arrangements for construction**3.11.1 Traffic management**

N/A

3.11.2 Service diversions

N/A

3.11.3 Interface with existing structures

N/A

4. DESIGN CRITERIA

4.1 Live loading , Headroom

4.1.1 Loading relating to normal traffic under AW regulations and C&U regulations

Full HA loading in accordance with BD 37/01

4.1.2 Loading relating to General Order traffic under STGO regulations

37.5 units of HB loading on any one notional lane only in accordance with BD 37/01

4.1.3 Footway or footbridge live loading

Verge loading in accordance with BD 37/01

4.1.4 Loading relating to Special Order Traffic, provision for exceptional abnormal loads or indivisible loads, including location of vehicle track on deck cross-section

N/A

4.1.5 Any special loading not covered above

Approach embankments founded on soft ground will be subjected to advance works surcharging and/or ground treatment eg piled platform, band drains or controlled modulus column installation, in advance of structural piling. Any residual lateral load or negative skin friction effects resulting from approach embankment loadings will be assessed and included in the design loadings for the bridge piled foundations.

4.1.6 Heavy or high load route requirements and arrangements being made to preserve the route, including any provision for future heavier loads or future widening.

N/A

4.1.7 Minimum headroom provided

The minimum headroom below bridge beams and in-situ deck slab shall not be less than 2.3m adjacent to the west abutment or 1.5m adjacent to the east abutment after allowing for deflections arising from dead load, live load and settlement.

In addition, the soffit level of the deck shall be at a level greater than or equal to the 100 year flood level +20% flood flow plus 600mm freeboard.

4.1.8 Authorities consulted and any special conditions required

Authority Consulted

1: British Telecom

2: EDF Energy

3: ESCC Planning

Special Requirement

1x90mm PVC duct required over structure.

1x150mm duct required over structure.

Planning Condition number 5. Bridge abutments are to be set back 2m from top

of waterway channel banks to facilitate green corridor and soft bank solution.

4. ESCC

1.5m minimum maintenance headroom to underside of structure.

5. Environment Agency

600mm freeboard to be provided above water level during 100yr return period flood + 20% flood flow.

4.2 List of relevant documents from the TAS

See Appendix A

4.2.1 Additional relevant standards

BS 8500; Part 1; 2006	Concrete; Complementary British Standard to BS EN 206-1; Method of specifying and guidance for the specifier
BS 8500; Part 2; 2006	Concrete; Complementary British Standard to BS EN 206-1; Specification for constituent materials and concrete
CHE Memorandum 227/08	The Impregnation of Reinforced and Prestressed Concrete Highway Structures Using Hydrophobic Pore Lining Impregnants

4.3 Proposed Departures from Standards given in 4.2 and 4.2.1

None

4.4 Proposed methods for dealing with aspects not covered by Standards in 4.2 and 4.2.1

N/A

5. STRUCTURAL ANALYSIS

5.1 Methods of analysis proposed for superstructure, substructure and foundations

The structure will be analysed in accordance with the recommendations given in PCA publication 'Integral abutments for prestressed beam bridges' by B.A Nicholson.

For the construction phase, the distribution of bending moments and shear forces in the deck will be determined by use of a simply supported line beam analysis.

For in service effects the deck analysis will be split into two stages. Firstly a grillage analysis will be undertaken assuming pinned supports at the abutments. The analysis will determine the maximum sagging moments in the deck, shear force distribution and vertical reactions. Transverse thermal and shrinkage effects will be considered in the design and appropriate measures taken to allow for these effects.

Secondly, a portal frame analysis of the deck and abutment stem walls will be undertaken, making allowance for the deck being monolithic with its supports and modelling soil structure interaction. The analysis will make allowance for the restraint to shrinkage and creep due to continuity over the supports. The analysis will return the maximum hogging moments in the deck and evaluate the rotation to be applied to the pile heads in the piled foundation design.

Load effects envelopes will be determined for the prestressed concrete beams which will be designed to Class 1 and Class 2 conditions.

Abutment stem walls will be designed for load effects determined from the portal frame analysis.

Retaining walls will be analysed by hand calculation.

Piled foundations will be analysed using appropriate industry standard software, considering a single representative pile and taking account of soil structure interaction effects including the lateral movements and rotational effects induced by deck load effects. Pile spacing is such that pile group effects are not considered to be appropriate. Torque effects from unbalanced earth pressure behind opposing abutments will be considered.

Additional lateral loading on piles arising from potential approach embankment settlement will be analysed and added to pile loads arising from the deck and abutment analyses.

5.2 Description and diagram of idealised structure to be used for analysis.

Refer to Appendix D for diagram of idealised structure(s).

5.3 Assumptions intended for calculation of structural element stiffness

Element stiffness for concrete members will be determined in accordance with BS5400; Part 4; 1990; Clause 4.4 using full elastic uncracked member cross sections ignoring the presence of reinforcement.

5.4 Proposed earth pressure coefficients (k_a , k_0 , or k_p) to be used in the design of earth retaining elements

Earth pressure coefficients used in the calculation of lateral earth pressures at the rear of a full-height frame integral abutment will be calculated in accordance with the requirements and recommendations contained in BA 42/96 'The Design of Integral Bridges'. The earth pressure coefficients used in the calculation of the 'K' and 'at rest' earth pressures at the rear of the abutment shall be based on upper bound 6N granular backfill properties of density = 22kN/m³, maximum $\phi' = 45^\circ$, $K_0 = 0.6$ and $K_p = 12.6$ when considering adverse effects.

The earth pressure coefficients used in the calculation of the earth pressures at the rear of the cantilever wingwalls will be based on the guidance presented in "Integral Abutments for Prestressed Beam Bridges" by BA Nicholson 1998.

For the analysis of the free standing earth retaining wingwalls a representative peak angle of friction of 35° will be used, for which $k_a = 0.27$; $k_p = 3.69$ and $k_0 = 0.43$ (calculated in accordance with BD 30/87). k_a will be used for stability calculations and k_0 for structural element design.

6. GEOTECHNICAL CONDITIONS

6.1 Acceptance of recommendations of Section 8 of the Geotechnical Report to be used in the design and reasons for any proposed changes.

Section 2 of the Geotechnical Report has not been completed at this stage.

6.2 Geotechnical Report Highway Structure Summary Information (Form C)

A draft Geotechnical Report Highway Structure Summary sheet based on the information available in Part 1 of the Geotechnical Report is attached in Appendix C. A full Geotechnical Report Highway Structure Summary sheet and extracts from the completed Geotechnical Report Section 2 will be produced following development of the Geotechnical Report.

6.3 Differential settlement to be allowed for in the design of the structure.

The structure is founded on piles extending to the Ashdown Formation. A maximum differential settlement of 10mm between abutments will be considered.

- 6.4 If the Geotechnical Report is not yet available, state when the results are expected and list the sources of information used to justify the preliminary choice of foundations.**

The preliminary choice of foundation is discussed in the draft Geotechnical Report Highway Structure Summary sheet contained in Appendix C. Part 2 of the Geotechnical Report, including Section 2 Highway Structures, is expected to be completed in Phase 2 of the project.

7. CHECKING

- 7.1 Proposed category of structure**

Category 2 in accordance with BD2/05

- 7.2 If Category 3, name of proposed Independent checkers.**

N/A

- 7.3 Erection proposals or temporary works for which an independent check will be required, listing parts of the structure affected with reasons for recommending an independent check.**

N/A

8. DRAWINGS AND DOCUMENTS

- 8.1 List of drawings and documents accompanying the submission.**

Appendix A List of relevant documents from TAS dated February 2009

Appendix B	Drawing No B1297000-PH2/1600.06a/9121	Title S12 Powdermill Stream Underbridge AIP General Arrangement
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Appendix C	Geotechnical Information	Draft Geotechnical Report Highway Structure Summary Sheet.
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Appendix D	Idealised Structure	
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9 THE ABOVE IS SUBMITTED FOR ACCEPTANCE

9.1 Submission by designer

Signed



Name: P Blackie
Position: Structures team leader, Jacobs
Engineering Qualifications: BEng (Hons), CEng MICE

Date 23/08/12

9.2 Endorsement by contractor

Signed

Name:

Engineering Qualifications:.....

Position:....., Hochtief Vinci Joint Venture

Date:

10. THE ABOVE IS REJECTED/AGREED SUBJECT TO THE AMENDMENTS AND CONDITIONS SHOWN BELOW.

Reviewed

Name:.....

Engineering qualifications.....

Date:

Signed

Name:.....

TAA

Engineering qualifications.....

Date:



Appendix A List of Relevant Documents

 Schedule of Design Documents Relating to Highway Bridges and Structures; February 2009
British Standards

BS 5268; Part 2; 2002	Structural Use of Timber
BS 5400	Steel concrete and composite bridges
Part 1; 1988	General Statement (see BD 1)
Part 2; 1978	Specification for loads (see BD 1)
Part 3; 2000	CP for design of steel bridges (see BD 1)
Part 4; 1990	CP for design of concrete bridges (see BD 2)
Part 5; 1979	CP for design of composite bridges (see BD 16)
Part 9; 1983	Bridge bearings (see BD 20)
Part 10; 1980	CP for fatigue (see BD 9)
BS 5628; Part 1; 1992	Unreinforced Masonry
BS 5930; 1999	Site Investigations
BS 6031; 1981	Earthworks
BS 8002; 1994	Earth retaining structures
BS 8004; 1986	Foundations
BS 8118; 1991	The structural use of aluminium
BS EN 1317-1-1998; Road Restraint Systems – Part 1	Terminology and general criteria for test methods
BS EN 1317-2-1998; Road Restraint Systems – Part 2	Performance classes, impact test acceptance criteria and test methods for safety barriers
BS EN 1317-3-2000; Road Restraint Systems – Part 3	Performance classes, impact test acceptance criteria and test methods for crash cushions
DD ENV 1317-4-2002; Road Restraint Systems – Part 4	Terminals and transitions
BS EN 14388; 2005	Road traffic noise reducing devices – Specification

Miscellaneous

Circular Roads No 61/72 – Routes for heavy and high abnormal loads.

Railway Group Approved Code of Practice GC/RC5510: Recommendations for the Design of Bridges (2000) (for full list of other Network Rail Standards, refer to RSSB, Railway Safety and Standards Board)

Simplified Tables of External Loads on Buried Pipelines (1986)

Traffic Management Act 2004

The Manual of Contract Documents for Highway Works (MCDHW)

Volume 1: Specification for Highway Works 1998, including amendments to November 2007

Volume 2: Notes for Guidance on the Specification for Highway Works 1998, including amendments to November 2007

Volume 3: Highway Construction Details 1991, including amendments to May 2007

The Design Manual for Roads and Bridges (DMRB)

Bridges and Structures (BA Series)

Reproduced on following pages

Bridges and Structures (BD Series)

Reproduced on following pages

Bridges and Structures, Technical Memoranda (BE Series)

Reproduced on following pages

Traffic Engineering and Control, Standards (TD Series)

TD 9/93	Road layout and geometry. Highway link design
TD 19/06	Requirement of Road Restraint Systems & correction No. 1
TD 27/05	Cross Sections and headroom
TD 36/93	Subways for pedestrians and cyclists, layout and dimensions

Highways, Advice Notes (HA Series)

HA 59/92	Mitigating Against Effects on Badgers
HA 65/94	Design Guide for Environmental Barriers
HA 66/95	Environmental barriers Technical Requirements
HA 80/99	Nature Conservation Advice in Relation to Bats
HA 84/01 (1)	Nature Conservation and Biodiversity
HA 97/01	Nature Conservation Management Advice in Relation to Dormice
HA 98/01	Nature Conservation Management Advice in Relation to Amphibians

Highways, Standards (HD Series)

HD 22/08	Managing Geotechnical Risk
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ADVICE NOTES - BRIDGES AND STRUCTURES (BA SERIES)

BA 9/81	The Use of BS 5400: Part 10: 1980. Code of Practice for Fatigue Amendment No. 1
BA 16/97	The Assessment of Highway Bridges and Structures. Amendment No. 1 Amendment No. 2
BA 19/85	The Use of BS 5400: Part 3: 1982
BA 24/87	Early Thermal Cracking of Concrete Amendment No. 1
BA 26/94	Expansion Joints for Use in Highway Bridge Decks
BA 28/92	Evaluation of Maintenance Costs in Comparing Alternative Designs for Highway Structures
BA 30/94	Strengthening of Concrete Highway Structures Using Externally Bonded Plates
BA 34/90	Technical Requirements for the Assessment and Strengthening Programme for Highway Structures
BA 35/90	Inspection and Repair of Concrete Highway Structures
BA 36/90	The Use of Permanent Formwork
BA 37/92	Priority Ranking of Existing Parapets
BA 38/93	Assessment of the Fatigue Life of Corroded or Damaged Reinforcing Bars
BA 39/93	Assessment of Reinforced Concrete Half-joints
BA 40/93	Tack Welding of Reinforcing Bars
BA 41/98	The Design and Appearance of Bridges
BA 42/96	The Design of Integral Bridges [Incorporating Amendment No. 1 dated May 2003]
BA 43/94	Strengthening, Repair and Monitoring of Post-tensioned Concrete Bridge Decks
BA 44/96	Assessment of Concrete Highway Bridge and Structures
BA 47/99	Waterproofing and Surfacing Concrete Bridge Decks
BA 50/93	Post-tensioned Concrete Bridges: Planning, Organisation and Methods for Carrying Out Special Inspections
BA 51/95	The Assessment of Concrete Structures Affected by Steel Corrosion
BA 52/94	The Assessment of Concrete Highway Structures Affected by Alkali Silica Reaction
BA 53/94	Bracing Systems and the Use of U-Frames in Steel Highway Bridges
BA 54/94	Load Testing for Bridge Assessment
BA 55/06	The Assessment of Bridge Substructures and Foundations, Retaining Walls and Buried Structures
BA 56/96	The Assessment of Steel Highway Bridges and Structures
BA 57/01	Design for Durability
BA 58/94	Design of Bridges and Concrete Structures with External Unbonded Prestressing
BA 59/94	Design of Highway Bridges for Hydraulic Action
BA 61/96	The Assessment of Composite Highway Bridges
BA 67/96	Enclosure of Bridges
BA 68/97	Crib Retaining Walls
BA 72/03	Maintenance of Road Tunnels

ADVICE NOTES - BRIDGES AND STRUCTURES (BA SERIES)

BA 74/06	Assessment of Scour at Highway Bridges
BA 80/99	Use of Rock Bolts
BA 82/00	Formation of Continuity Joints in Bridge Decks
BA 83/02	Cathodic Protection for Use in Reinforced Concrete Highway Structures
BA 84/02	Use of Stainless Steel Reinforcement in Highway Structures
BA 85/04	Coatings for Concrete Highway Structures & Ancillary Structures
BA 86/06	Advice Notes on the Non-Destructive Testing of Highway Structures
BA 87/04	Management of Corrugated Steel Buried Structures
BA 88/04	Management of Buried Concrete Box Structures
BA 92/07	The Use of Recycled Concrete Aggregates in Structural Concrete
BA 93/09	Structural Assessment of Bridges with Deck Hinges

STANDARDS - BRIDGES AND STRUCTURES (BD SERIES)

BD 2/05	Technical Approval of Highway Structures
BD 7/04	Weathering Steel for Highway Structures
BD 9/84	Implementation of BS 5400: Part 10: 1980. Code of Practice for Fatigue
BD 10/97	Design of Highway Structures in Areas of Mining Subsidence
BD 12/01	Design of Corrugated Steel Buried Structures with Spans Greater than 0.9 Metres and up to 8.0 Metres
BD 13/06	Design of Steel Bridges. Use of BS 5400: Part 3: 2000
BD 15/92	General Principles for the Design and Construction of Bridges. Use of BS 5400: Part 1: 1988
BD 16/82	Design of Composite Bridges. Use of BS 5400: Part 5: 1979 Amendment No. 1
BD 20/92	Bridge Bearings. Use of BS 5400: Part 9: 1983
BD 21/01	The Assessment of Highway Bridges and Structures
BD 24/92	Design of Concrete Bridges. Use of BS 5400: Part 4: 1990
BD 27/86	Materials for the Repair of Concrete Highway Structures
BD 28/87	Early Thermal Cracking of Concrete Amendment No. 1
BD 29/04	Design Criteria for Footbridges
BD 30/87	Backfilled Retaining Walls and Bridge Abutments
BD 31/01	The Design of Buried Concrete Box and Portal Frame Structures
BD 33/94	Expansion Joints for Use in Highway Bridge Decks
BD 34/90	Technical Requirements for the Assessment and Strengthening Programme for Highway Structures
BD 35/06	Quality Assurance Scheme for Paints and Similar Protective Coatings
BD 36/92	Evaluation of Maintenance Costs in Comparing Alternative Designs for Highway Structures
BD 37/01	Loads for Highway Bridges

STANDARDS - BRIDGES AND STRUCTURES (BD SERIES)

BD 41/97	Reinforced Clay Brickwork Retaining Walls of Pocket Type and Grouted Cavity type Construction Use of BS 5628: Part 2: 1995
BD 42/00	Design of Embedded Retaining Walls and Bridge Abutments
BD 43/03	The Impregnation of Reinforced and Prestressed Concrete Highway Structures using Hydrophobic Pore-Lining Impregnants
BD 44/95	The Assessment of Concrete Highway Bridges and Structures
BD 45/93	Identification Marking of Highway Structures
BD 46/92	Technical Requirements for the Assessment and Strengthening Programme for Highway Structures [Stage 2—Modern Short-Span Bridges]
BD 47/99	Waterproofing and Surfacing of Concrete Bridge Decks
BD 48/93	The Assessment and Strengthening of Highway Bridge Supports
BD 49/01	Design Rules for Aerodynamic Effects on Bridges
BD 50/92	Technical Requirements for the Assessment and Strengthening Programme for Highway Structures Stage 3—Long-Span Bridges
BD 51/98	Portal and Cantilever Signs/Signal Gantries
BD 53/95	Inspection and Records for Road Tunnels
BD 54/93	Post-tensioned Concrete Bridges, Prioritisation of Special Inspections
BD 56/96	The Assessment of Steel Highway Bridges and Structures
BD 57/01	Design for Durability
BD 58/94	The Design of Concrete Highway Bridges and Structures with External and Unbonded Prestressing Design of Highway Bridges for Vehicle Collision Loads
BD 60/04	Design of Highway Bridges for Vehicle Collision Loads
BD 61/96	The Assessment of Composite Highway Bridges
BD 62/07	As Built, Operational and Maintenance Records for Highway Structures
BD 63/07	Inspection of Highway Structures
BD 65/97	Design Criteria for Collision Protector Beams
BD 67/96	Enclosure of Bridges
BD 68/97	Crib Retaining Walls
BD 70/03	Strengthened/Reinforced Soils and Other Fills for Retaining Walls and Bridge Abutments Use of BS8006: 1995, incorporating Amendment No. 1 (Issue 2 March 1999)
BD 74/00	Foundations
BD 78/99	Design of Road Tunnels
BD 79/06	The Management of sub-Standard Highway Structures
BD 81/02	Use of Compressive Membrane Action in Bridge Decks
BD 82/00	Design of Buried Rigid Pipes
BD 84/02	Strengthening of Concrete Bridge Supports Vehicle Impact Using Fibre Reinforced Polymers
BD 85/08	Strengthening Highway Structures Using Externally Bonded Fibre Reinforced Polymer
BD 86/07	The Assessment of Highway Bridges and Structures For The Effects of Special Types General Order (STGO) and Special Order (SO) Vehicles
BD 87/05	Maintenance Painting of Steelwork

STANDARDS - BRIDGES AND STRUCTURES (BD SERIES)

BD-89/03	The Conservation of Highway Structures
BD-90/05	Design of FRP Bridges and Highway Structures
BD-91/04	Unreinforced Masonry Arch Bridges
BD-94/07	Design of Minor Structures
BD-95/07	Treatment of Existing Structures on Highway widening Schemes

TECHNICAL MEMORANDA - BRIDGES (BE SERIES)

BE-13	Fatigue Risk in Bailey Bridges
BE-23	Shear Key Decks Amendment No. 1 to Annex
BE-5/75	Rules for the Design and Use of Freyssinet Concrete Hinges in Highway Structures
BE-7/04	Departmental Standard (Interim) Motorway Sign/Signal Gantries

INTERIM ADVICE NOTES (IAN)

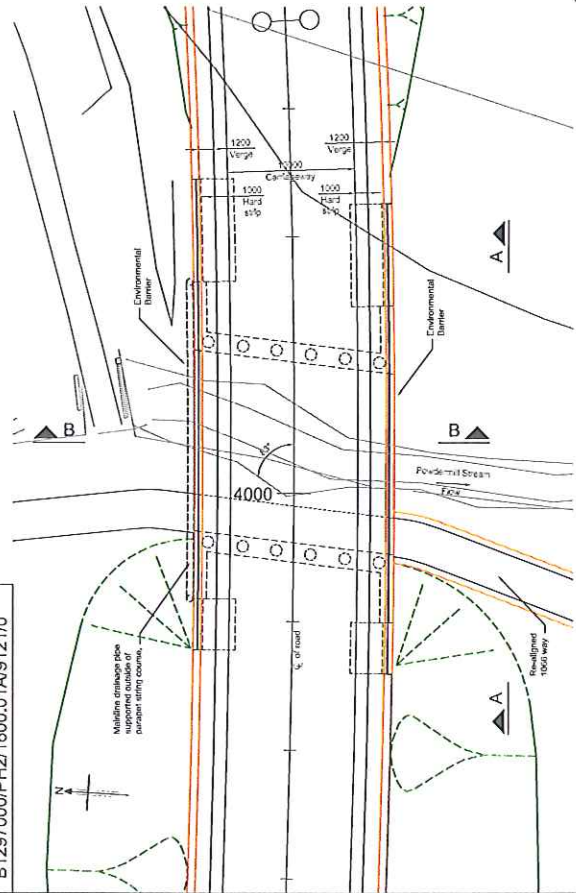
IAN-117/08 Rev 1	Certification of combined kerb and drainage products
IAN-116/08	Nature conservation advice in relation to bats
IAN 104/07	The Anchorage of Reinforcement and Fixings in Hardened Concrete
IAN-97/07	Assessment and upgrading of existing parapets
IAN 96/07r1	Guidance on implementing Results of Research on Bridge Deck Waterproofing
IAN 95/07	Revised Guidance Regarding the Use of BS8500(2006) For the Design and Construction of Structures Using Concrete
IAN-91/07	Interim Advice on the identification of "Particularly at Risk" supports
IAN 70/06	Implementation of New Reinforcement Standards
IAN 69/05	Design for Maintenance
IAN 48/03	Measures To Minimise The Risk of Sulphate Attack (Including Thaumasite) - New Construction and Structures Under Construction
IAN-47/02	Post-Tensioned Grouted Duct concrete Bridges
IAN 41/02	European Cement Standards
IAN 05/96	BD 24/92 The Design of Concrete Highway Bridges and Structures. Use of BS 5400: Part 4:1990
IAN-04/96	BD-44/95 The Assessment of Concrete Highway Bridges and Structures
IAN-03/96	BA-50/93 Post-Tensioned concrete Bridges

Appendix B Drawings

Drawing No
B1297000-PH2/1600.06a/9121

Title
S12 Powdermill Stream Underbridge
AIP General Arrangement

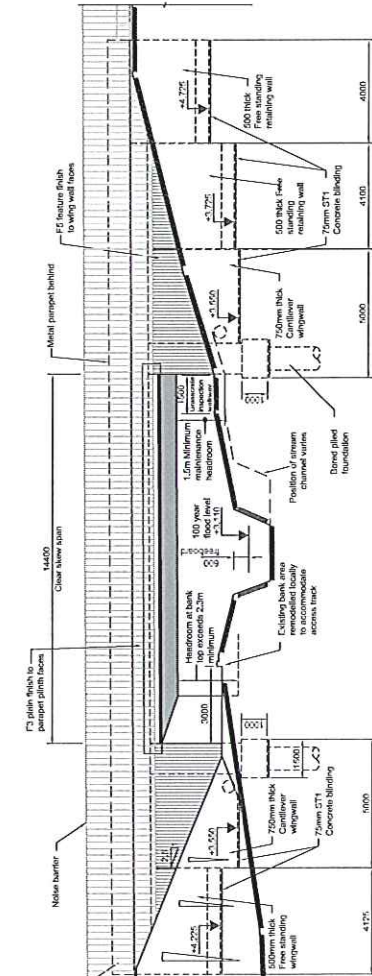
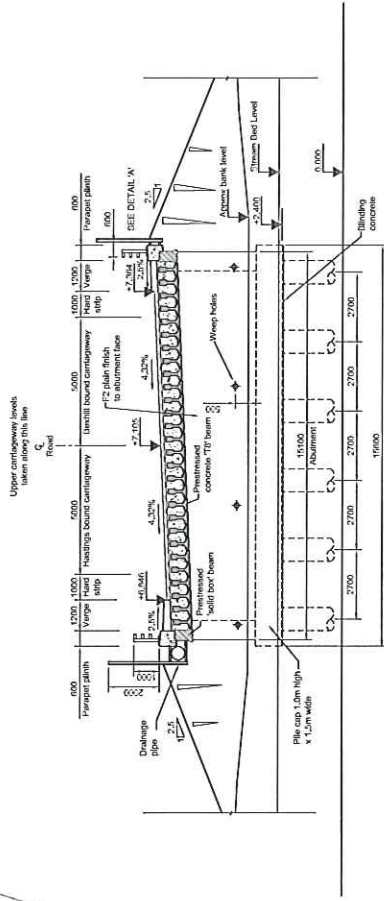
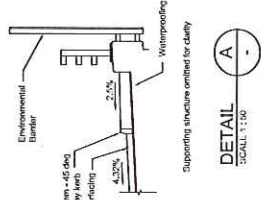
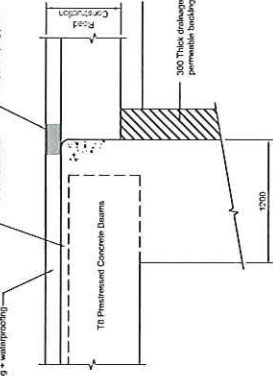
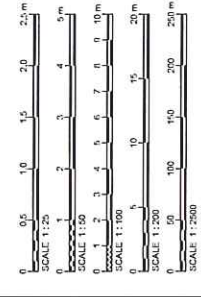
Drawing Number: B1297000/PH2/1600.01A/9121/0



- ### NOTES
- All dimensions in millimetres unless noted otherwise.
 - All levels in means A.O.D. (Above Ordnance Datum - Newlyn).
 - Do not scale from this drawing.
 - Dashed lines to be ON or OFF.
 - All external surfaces to have 25 x 25mm chamfers.
 - Columns shall be supported in the rock by abutments, immediately to the east (UPRIL) side of the bridge to prevent the flow of surface water across the pavement / abutment formation.
 - Approach embankments constructed in advance of bridge works. Ground treatment below approach embankments to limit differential settlements where necessary.
 - Both abutments to be identified simultaneously with a level difference not exceeding 10mm.
 - All section thicknesses are approximate and subject to change at detailed design stage.
 - Dimensions are square to abutments unless noted otherwise.

FULLY INTEGRATED ABUTMENT DECK CONNECTION

SCALE 1:25



Rev	Date	By	Checked	Approved
0	JAN 2017	JKH/AM	AM	AM

JACOBS
Engineering and Construction

HOCHTIEF/VINCI JOINT VENTURE
EAST SUSSEX COUNTY COUNCIL

**BEXHILL TO HASTINGS LINK ROAD
POWDERMILL STREAM
UNDERBRIDGE
GENERAL ARRANGEMENT
OPTION 2**

Client: HOCHTIEF/VINCI JOINT VENTURE
Project: BEXHILL TO HASTINGS LINK ROAD
Drawing Title: POWDERMILL STREAM UNDERBRIDGE GENERAL ARRANGEMENT OPTION 2

Drawing Status: FOR INITIAL COMMENT
Scale: AS SHOWN ON A3
Do Not Scale: DO NOT SCALE

Drawing Number: B1297000-PH2/1600.01A/9121/0
Revision: 0

This drawing is not to be used in whole or part other than for the intended purpose and project as defined in this drawing. Refer to the contract for full terms and conditions.

Information for the Contractor to be provided to the Contractor before the start of work. The Contractor shall be responsible for the interpretation of the drawing and shall ensure that the work is carried out in accordance with the contract and the relevant clauses of the contract.

Appendix C Geotechnical Information

BEXHILL TO HASTINGS LINK ROAD
GEOTECHNICAL SUMMARY INFORMATION

STRUCTURE NAME	CHAINAGE and OS Grid Reference	
S12 Powdermill Stream Underbridge	Ch 4000 OS: 576055.7E, 110582.6N	
Rev: 2	DESIGN LIFE: 120 years	
SOILS/GEOLOGY	RELEVANT EXPLORATORY HOLES:	
	BH147, BH148 (URS Investigation 2009)	
	BH16 (May Gurney, 2006)	
Strata	Typical depths	
Alluvium ¹	5.56 to 3.56m OD	
Ashdown Formation	below 3.56m OD	
PREVIOUS GROUND HISTORY	Agricultural land	
CONTAMINATED GROUND RISK ASSESSMENT REQUIRED	TBA	
GROUNDWATER		
<p>In BH147, groundwater was encountered at a level of -0.63m OD (5.1m bgl) within the Ashdown Formation layer and rose to 2.47m OD (2.0m bgl). Groundwater was encountered in BH148 initially at level -4.56m OD (1.0m bgl) within the Alluvium. A second groundwater strike encountered confined groundwater at level 1.66m OD (3.90m bgl) within Ashdown Formation and rose to 4.06m OD (1.50m bgl) in 20 minutes.</p> <p>In BH16 groundwater was encountered initially at 2.62m OD (4.1m bgl) within Ashdown Formation and rose to a level of 4.12m OD (2.6m bgl) in 20 minutes. . A second groundwater strike encountered confined groundwater within Ashdown Formation at -2.78m OD (9.7m bgl) and rose to a level of 3.47m OD (3.25m bgl) in 20 minutes. Groundwater monitoring carried out between April 2006 and March 2010 indicates a level of upto 1.3m bgl.</p> <p>For preliminary design, groundwater level is assumed at ground level.</p>		
EARTH PRESSURE VALUE K_0^* K_a^* K_p^*		
Refer to Section 5.4 of AIP.		
TYPE OF FOUNDATION	Piled foundation	
BEARING CAPACITY	Not used	





Structure Element	Founding Stratum	Founding Level (m OD)	Footing Size	Allowable Bearing Pressure (kN/m ²)	
PILE DESIGN					
Structure Element	Founding Stratum	Toe Level (m OD)	Pile dia (m)	Pile length (m)	Pile working Load (kN)
East Abutment	Ashdown Formation	-10.6	0.9	13	1750
West Abutment	Ashdown Formation	-10.6	0.9	13	1750
<p>Note: Pile lengths and toe levels are approximate.</p> <p>Pile type: Bored / CFA</p> <p>Criteria for selecting pile toe level: Pile capacity</p> <p>Allowance for negative skin friction within design: Yes</p>					
SETTLEMENT					
Differential settlement to be allowed for between adjacent supports: 10mm					
Differential settlement to be allowed between structure and approach embankment : 20mm (within 10 metres of the interface between structures and approach embankments)					
CHEMICAL ANALYSIS					
<p>Buried Concrete classification:</p> <p>The results of chemical tests on soil samples taken within the rural areas indicate pH values ranging between 3.8 to 9.4 and sulfates (2:1 Water Extract) values of between 10 to 900mg/l. The recommended Design Sulfate and Concrete Classification based on BRE Special Digest 1 (2005) are DS-2 and AC-3z respectively.</p>					
NOTES					

1. The Alluvium thickness has been increased to include soft Clay in Ashdown Formation.
2. The existing ground level ranges between 4.47 – 5.56m OD. The ground sequence at the site is Made Ground/Alluvium and Ashdown Formation. The available information from boreholes indicates Ashdown Formation layer at 1.0m bgl to 1.5m bgl. BH 148 indicates presence of weak Sandstone approximately 4.5m bgl.
3. Based on the formation level, the structure will likely be founded on Made Ground and soft Alluvium layer, which is underlain by soft/firm to very stiff interbedded sands, silts and clays of the Ashdown Formation. The unpredictable bearing behaviour of Made Ground and the low shear strength of the Alluvium layer prevent the use of these layers as a bearing stratum due to the risk of excessive settlements and failure. The maximum thickness of the Made Ground encountered in exploratory holes local to the proposed structure is 1.4m. The maximum thickness of Alluvium encountered local to the proposed structure is 1m. Hence, the load due to the structure will need to be transferred to the competent stiff to very stiff /very weak to weak interbedded Ashdown Formation. Thus, pile foundations are recommended

Syke BEXHILL BOREHOLE LOG File: J:\BIDFORD-JOB\EAST SUSSEX COUNTY COUNCIL\W03277 BEXHILL TO HASTINGS LINK ROAD\TECHNICAL\FACTUAL REPORT DATA\BIDFORD-BEXHILL - HASTINGS URS ALLOP1 PrintNo: 14/03/2009 12:30:29
 URS Corporation, Ltd Home Lane, Bideford, Devon, TIS Telephone: 01254 36641 www.urscorp.com

Contract No: 49325727
 Project: Bexhill - Hastings Link Road
 Client: East Sussex County Council


 Record of Borehole
BH147

SAMPLES & In situ TESTS			STRATA						
Depth	Type/ No.	SPT/U4 (Blows)	Water	Reduced Level (mOD)	Legend	Depth (Thickness)	DESCRIPTION	Instrument/ Backfill	
0.30	D1			4.37		0.10	Firm dark brown topsoil. (TOPSOIL)		
0.50	D2								White reworked silty chalk gravel fill. Gravel is subangular fine to coarse. (MADE GROUND)
1.00	D3 U4	(35 - 450mm)		3.67		0.80	Soft to firm grey-brown mottled orange-brown slightly gravelly clayey silt with fine fragments of coal and brick. Gravel is sub-rounded fine to coarse chalk and flint. (MADE GROUND)		
1.50	D5			2.97		1.50	Firm to stiff light grey and orange-brown very slightly gravelly SILT. Gravel is weak orange-brown and dark brown subangular fine to coarse siltstone. (Zone II) (ASHDOWN BEDS)		
2.00	D6 U7	(70 - 450mm)							At 2.5m bgl occasional black mottling.
2.50	D8 SPT9	N=12 (2/2/2/2/4/4)		1.57			2.90		Firm laminated light grey stained orange-brown slightly clayey SILT. Light grey silt partings. Laminations are orange-brown stained. (Zone III) (ASHDOWN BEDS)
3.00	D10 U11	(90 - 450mm)							Fissured light grey SILT with orange-brown staining along fissure surfaces at 3.5 m bgl.
3.50	D12						Stiff laminated light grey stained orange-brown slightly clayey SILT. Light grey silt partings. Laminations are orange-brown stained at 4.0m bgl.		
4.00	D13 U14	(100 - 450mm)					At 4.5 m bgl very stiff extremely to very closely fissured orange-brown and dark brown stained yellow brown SILT. Staining is along fissure surfaces.		
4.50	D15 SPT16	N=89 (7/18/25/25/20/19)					With occasional lithorelics/gravel of very weak grey stained orange-brown subangular fine to coarse siltstone at 5.0 m bgl.		
5.00	D17 U18 W24 D19	(Refused -)			-0.63		5.10		Very weak to weak grey and orange-brown slightly weathered SILTSTONE. Discontinuities appear to be extremely close to very closely spaced. (Zone II) (Recovered as subangular fine to coarse silty gravel.) (ASHDOWN BEDS)
5.10					-1.03		5.50		Very stiff light grey stained orange-brown SILT. (Zone III to II) (ASHDOWN BEDS)
6.00	SPT20	N=>100 (18/7/40/45/15/20mm/-)							Fissured at 6.0 m bgl.
6.50	D21								
7.00	SPT22	N=>100 (25/40mm/-/50/50/25mm/-/-)			-2.53		7.00		Weak orange-brown SILTSTONE/SANDSTONE. (Zone II) (Recovered as orange-brown slightly sandy silt. Sand is fine to coarse.) (ASHDOWN BEDS)
7.50	D23			-2.83		7.30	Very stiff light grey SILT. (Zone III to II) (ASHDOWN BEDS)		

Boring Progress and Water Observations									Chiselling			Water Added		GENERAL REMARKS
Date	Time	Hole Depth	Cas'g Depth	Cas'g Dia	Water Depth	Rose to	Time (mins)	Sealed (m)	From	To	Time (hh:mm)	From	To	
									5.10	5.50	01:00			
									7.00	7.30	01:00			

Draft
 Hand dug inspection pit to 1.2m bgl.
 Fast inflow of groundwater at 5.0mbgl.
 Slow inflow of groundwater after strike despite depth of casing.
 Zone of weathering interpreted from Spinks et al. 1993: (V); (IV); (III); (II); (I).

Logged by: JB Checked by: CAB Status: Draft	Equipment: Cable Percussion Rig - Dando 2000 Contractor: Southern Testing Laboratories Ltd	Location: 576183.1 E 110672.8 N	Ground Level: 4.47 mAOD	Date: 05/03/2009 Start 06/03/2009 End	Scale: 1:40.0 Sheet 1 of 3
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 URS Corporation Ltd Home Lane Bedford MK40 1TS Telephone: 01234 340641 www.URS.com

Contract No: 49325727
Project: Bexhill - Hastings Link Road
Client: East Sussex County Council


 Record of Borehole
BH147

SAMPLES & In situ TESTS			STRATA					
Depth	Type/No.	SPT/U4 (Blows)	Water	Reduced Level (mOD)	Legend	Depth (Thickness)	DESCRIPTION	Instrument/Backfill
8.00	SPT25	N=62 (7/18/13/13/16/20)					At 7.5 m bgl, recovered with brown-grey stained orange-brown slightly sandy SILT. Sand is fine to medium.	Instrument/Backfill
8.50	D26					Laminated at 8.5 m bgl.		
9.00	SPT27	N=37 (7/7/6/10/10/11)						
9.50	D28							
10.00	SPT29	N=59 (8/7/7/12/20/20)				Becoming dark grey at 10.0 m bgl.		
11.00	D30			-6.53		11.00	Very stiff fissured occasionally laminated grey SILT with occasional very slightly sandy grey silt partings. Sand is fine. (Zone II) (ASHDOWN BEDS)	
11.50	SPT31	N=28 (3/4/5/5/7/11)						
12.00	D32							
13.00	D33 U34	(150 - 150mm)						
13.50	SPT35	N=65 (11/14/15/15/15/20)						
14.50	D36							
15.00	SPT37							

Boring Progress and Water Observations									Chiselling			Water Added		GENERAL REMARKS
Date	Time	Hole Depth	Cas'g Depth	Cas'g Dia	Water Depth	Rose to	Time (mins)	Sealed (m)	From	To	Time (hh:mm)	From	To	
05/03/09	00.00	11.00	8.00	150	2.10				14.90	15.20	00:45			

Draft
 Hand dug inspection pit to 1.2m bgl. Fast inflow of groundwater at 5.0mbgl. Slow inflow of groundwater after strike despite depth of casing. Zone of weathering interpreted from from Spinks et al. 1993: (V); (IV); (III); (II); (I).

Logged by: JB Checked by: CAB Status: Draft	Equipment: Cable Percussion Rig - Dando 2000 Contractor: Southern Testing Laboratories Ltd	Location: 576183.1 E 110672.8 N	Ground Level: 4.47 mAOD	Date: 05/03/2009 Start 06/03/2009 End	Scale: 1:40.0 Sheet 2 of 3
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SHE: BEXHILL BOREHOLE LOG File: J:\BEPORD\JES\BEXHILL TO HASTINGS LINK ROAD\TECHNICAL\ACTUAL REPORT DATA\BEXHILL - HASTINGS URS ALL.DWG Printed: 14/06/2009 13:35:31

URS Corporation Ltd Home Lane Bedford MK40 1TS Telephone: 01234 546644 www.URSCon.com

Contract No: 49325727
Project: Bexhill - Hastings Link Road
Client: East Sussex County Council











Record of Borehole
BH147

SAMPLES & In situ TESTS			STRATA					Instrument/ Backfill
Depth	Type/ No.	SPT/U4 (Blows)	Water	Reduced Level (mOD)	Legend	Depth (Thick- ness)	DESCRIPTION	
15.20	SPT38			-10.78	x x	15.25	End of Borehole at 15.25m	

Boring Progress and Water Observations									Chiselling			Water Added		GENERAL REMARKS
Date	Time	Hole Depth	Cas'g Depth	Cas'g Dia	Water Depth	Rose to	Time (mins)	Sealed (m)	From	To	Time (hh:mm)	From	To	
06/03/09	00.00	15.25	8.00	150	1.90									Draft Hand dug inspection pit to 1.2m bgl. Fast inflow of groundwater at 5.0mbgl. Slow inflow of groundwater after strike despite depth of casing. Zone of weathering interpreted from from Spinks et al. 1993: (V); (IV); (III); (II);(I).
Logged by: JB		Equipment: Cable Percussion Rig - Dando 2000			Location: 576183.1 E 110672.8 N		Ground Level: 4.47 mAOD		Date: 05/03/2009 Start 06/03/2009 End		Scale: 1:40.0		Sheet 3 of 3	
Checked by: CAB		Contractor: Southern Testing Laboratories Ltd												
Status: Draft														

S:\M - BEXHILL BOREHOLE LOG File: J:\BEDFORD-JOIST\CAST SUSSEX COUNTY COUNCIL\49325727 BEXHILL TO HASTINGS LINK ROAD\TECHNICAL\ACTUAL REPORT DATA\BEXHILL - HASTINGS URS ALL.DWG Printed: 14/02/2009 13:30:33
 URS Corporation Ltd Home Lane Bedford MK40 1TD Telephone: 01234 249641 www.URS.com

Contract No: 49325727		 Record of Borehole BH148
Project: Bexhill - Hastings Link Road		
Client: East Sussex County Council		


SAMPLES & In situ TESTS			STRATA					
Depth	Type/ No.	SPT/U4 (Blows)	Water	Reduced Level (mOD)	Legend	Depth (Thickness)	DESCRIPTION	Instur- ment/ Backfill
0.50	D1		↓			(1.00)	Very soft, dark brown, peaty CLAY, with frequent, fine to medium, firm, fibrous, organic matter fragments, and occasional, fine to medium sub-rounded to sub-angular flint gravel gravels. (ALLUVIUM)	Instur- ment/ Backfill
1.00	D2			4.56		1.00	Soft, orange/brown and grey mottled sandy CLAY, with frequent, randomly orientated, fine to coarse, angular to sub-angular lithorelics of sandstone and mudstone, and rare fine rooflets. (ASHDOWN BEDS)	
1.50	U3	(30 - 350mm)	↓			(1.00)		
2.00	D4			3.56		2.00	Stiff, closely fissured, orange/brown and grey mottled sandy CLAY, with occasional heavy iron-staining present along fissures. (ASHDOWN BEDS)	
2.50	U5	(45 - 450mm)	↓					
2.70				2.86		2.70		
3.00	D6 SPT7	N=19 (2/2/5/4/5/5)	↓					
3.50	U8	(36 - 450mm)				(1.00)	Stiff, closely fissured, grey, mottled orange/brown CLAY, with heavy iron-staining present along fissures, and rare, up to 5mm randomly orientated lithorelics of weak, weathered, mudstone. (ASHDOWN BEDS)	
4.00	D9 W10		↓			3.90		
4.50	SPT11	N=10 (1/0/1/2/4/3)		1.66			Interbedded SANDSTONE and MUDSTONE recovered as soft, grey and orange/brown sandy clay, with frequent fine to coarse angular gravels of weak to medium strong, highly-weathered, heavily iron-stained, thinly colour laminated sandstone. (ASHDOWN BEDS)	
5.50	SPT12	N=53 (12/13/50mm/20/13/10/10)	↓					
5.70	D13			0.16		5.40	Very weak, light grey, orange/brown mottled, weathered, fine-grained SANDSTONE. Recovered as a fine-grained sand with frequent, medium to coarse gravels of grey, orange/brown, mottled sandstone (poor quality sample). (ASHDOWN BEDS)	
6.50	U14	(100 - 300mm)	↓					
7.00	D15			-1.44		7.00	Very stiff, very closely fissured, dark grey CLAY, with occasional partings of light grey silt and some dark orange iron-staining present along fissures. (ASHDOWN BEDS)	
7.50	U	(100 - 0mm)						

Boring Progress and Water Observations									Chiselling			Water Added		GENERAL REMARKS
Date	Time	Hole Depth	Cas'g Depth	Cas'g Dia	Water Depth	Rose to	Time (mins)	Sealed (m)	From	To	Time (hh:mm)	From	To	
22/01/09	14.00	1.00	0.00		1.00				5.40	5.50	00:15			
22/01/09	15.30	3.90	3.30	150	3.90	1.50	20							
22/01/09	16.15	5.70	5.30	150	2.50									
23/01/09	08.00	5.70	5.70	150	0.10									

Logged by: HH Checked by: CAB Status: Draft	Equipment: Cable Percussion Rig - Dando 2000 Contractor: Southern Testing Laboratories Ltd	Location: 576199.1 E 110677.0 N	Ground Level: 5.56 mAOD	Date: 22/01/2009 Start 23/01/2009 End	Scale: 1:40.0 Sheet 1 of 2
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Draft.
 150mm casing to 7.2m bgl.
 No visual or olfactory evidence of contamination encountered.
 Chiselling from 10.4-10.5m bgl and 10.5-10.7m bgl.
 Fast groundwater inflow at 3.9mbgl.
 Seepage at 1.0m bgl.
 Zone of weathering interpreted from from Spinks et al. 1993: (V); (IV); (III); (II); (I).

Site: BEXHILL BOREHOLE LOG File: J:\BEDFORD-JOB\BEXHILL TO HASTINGS LINK ROAD\TECHNICAL\ACTUAL REPORT DATA\BEXHILL - HASTINGS URS ALLOP1 - Prime: 14092009 12:30:39

Contract No: 49325727		 Record of Borehole BH148
Project: Bexhill - Hastings Link Road		
Client: East Sussex County Council		

SAMPLES & In situ TESTS			STRATA					
Depth	Type/ No.	SPT/J4 (Blows)	Water	Reduced Level (mOD)	Legend	Depth (Thickness)	DESCRIPTION	instru- ment/ Backfill
8.00	B16 SPT17	N=>100 (8/17/65mm/25/30/35/10/20mm)		-2.14	---	7.70	Poor recovery from 7.5m bgl; clay becoming softer and lighter in colour. Orange staining becoming more frequent along fissures. Very dense, light grey, slightly clayey, silty SAND, with rare, dark orange, iron staining. (ASHDOWN BEDS)	Backfill
9.00	SPT18	N=85 (6/8/10/20/25/30)			.		Becoming a silty SAND from 9.0m bgl.	
10.00	SPT19	N=>100 (5/10/30mm/16/18/30/36/50mm)		-4.44	x x x x	10.00	Very dense, closely fissured light grey SILT, with rare, dark orange, iron staining. (ASHDOWN BEDS)	
				-4.84	x x x x	10.40	Very weak, closely fractured, weathered, light grey SILTSTONE, with occasional, dark orange iron staining present along fractures. (ASHDOWN BEDS)	
10.70	SPT20	N=>100 (10/15/30mm/20/27/33/20/40mm)		-5.14	x x x x	10.70	End of Borehole at 10.70m	

Boring Progress and Water Observations									Chiselling			Water Added		GENERAL REMARKS
Date	Time	Hole Depth	Cas'g Depth	Cas'g Dia	Water Depth	Rose to	Time (mins)	Sealed (m)	From	To	Time (hh:mm)	From	To	
23/01/09	13.00	10.70	7.20	150	2.00				10.50	10.70	01:00			

Draft.
150mm casing to 7.2m bgl.
No visual or olfactory evidence of contamination encountered.
Chiselling from 10.4-10.5m bgl and 10.5-10.7m bgl.
Fast groundwater inflow at 3.9mbgl.
Seepage at 1.0m bgl.
Zone of weathering interpreted from Spinks et al. 1993: (V); (IV); (III); (II); (I).

Logged by: HH Checked by: CAB Status: Draft	Equipment: Cable Percussion Rig - Dando 2000 Contractor: Southern Testing Laboratories Ltd	Location: 576199.1 E 110677.0 N	Ground Level: 5.56 mAOD	Date: 22/01/2009 Start 23/01/2009 End	Scale: 1:40.0 Sheet 2 of 2
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URS Corporation Ltd Home Lane Bedford MK40 1TS Telephone: 01234 49041 www.URS.com




MAY GURNEY			Site Bexhill to Hastings Link Road	Borehole Number BH16
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Boring Method Cable Percussion	Casing Diameter 150mm cased to 7.00m	Ground Level (mOD) 6.72	Client East Sussex County Council	Job Number SI1085
	Location 576201.473 E 110629.515 N	Dates 08/03/2006-09/03/2006	Engineer Owen Williams	Sheet 1/3

Depth (m)	Sample / Tests	Casing Depth (m)	Water Depth (m)	Field Records	Level (mOD)	Depth (m) (Thickness)	Description	Legend	Water	Instr
0.30-0.80	B1				6.42	(0.30)	TOPSOIL. Firm brown slightly gravelly sandy CLAY. Gravel is angular to subrounded fine and medium flint.			
0.80-1.20	B2				5.92	0.80	Firm mottled orange brown and light brown sandy SILT / CLAY.			
1.50	U1			32 blows						
1.95-2.00-2.50	D1 B3									
2.50-2.95-2.50	SPT N=19 D2	1.30		2,2/3,6,5,5		(3.70)			▽1	
3.50-3.50-3.95	U2 D3			50 blows					▽2	
4.00-4.50-4.10	B4 W1			FAST(1) at 4.10m, rose to 2.55m in 20 mins, sealed at 7.00m.					▽1	
4.50-4.50-4.87	D4 SPT 50/220	2.90	2.90	7,10/14,20,16	2.22	4.50	Very stiff mottled brown and grey SILT			
5.50	U3			100 blows		(2.50)				
6.00-6.50	B5									
6.50-6.95-6.50-6.95	SPT N=45 D5	5.90	4.80	14,11/10,8,11,16						
7.50-7.50	D6 U4			50 blows						
8.00-8.50	B6									
8.50-8.95-8.50-8.95	SPT N=50 D7	7.00		6,7/10,12,12,16						
9.50-9.50-9.70	D8 U5 W2			FAST(2) at 9.70m, rose to 3.30m in 100 blows 20 mins.	-0.28	7.00	Very stiff light grey CLAY with pockets of orange and brown fine sand.		▽2	

Remarks Hand excavated pit to 1.20m 50mm diameter standpipe installed with raised cover protected with fence PID reading adjacent to BH at 0.30m bgl = 0.4ppm Water added from 1.50m to 4.10m. Water added from 7.00m to 9.70m.	Scale (approx) 1:50	Logged By JE/AK
	Figure No. SI1085.BH16	

						Site		Borehole Number		
Boring Method Cable Percussion		Casing Diameter 150mm cased to 7.00m		Ground Level (mOD) 6.72		Client East Sussex County Council		Job Number SH1085		
		Location 576201.473 E 110629.515 N		Dates 08/03/2006-09/03/2006		Engineer Owen Williams		Sheet 2/3		
Depth (m)	Sample / Tests	Casing Depth (m)	Water Depth (m)	Field Records	Level (mOD)	Depth (m) (Thickness)	Description	Legend	Water	Instr
10.00-10.50	B8									
10.50-10.95 10.50-10.95	SPT N=53 D9	7.00	3.30	12,13/16,14,10,13						
11.50 11.50	D10 U6			100 blows						
12.50-12.80 12.50	SPT 50/150 D11	12.50	3.70	11,14/22,28		(9.00)				
13.50 13.50	D12 U7			100 blows						
13.95	D13									
14.50-14.82 14.50 14.50-15.00	SPT 50/170 D14 B9	14.50	3.90	15,10/20,19,11						
15.50 15.50 15.50-15.95	D15 U8 B10			100 blows						
16.00-16.50	B11				-9.28	16.00	Weak SILTSTONE and brown COAL recovered as a grey and black sandy SILT. Gravel is angular to subangular fine to medium brown coal			
16.50-16.95 16.50 16.50-16.95	SPT N=50 D16 D17	16.30	4.10	6,9/9,10,14,17		(2.00)				
17.50 17.50	D18 U9			150 blows						
18.00-18.50	B12				-11.28	18.00	Weak SILTSTONE recovered as a slightly sandy SILT with occasional bands of coal.			
18.50-18.70 18.50	SPT 25*/80 50/115 D19	18.40	4.50	20,5/28,22		(2.15)				
19.50 19.50 20.00-20.14	D20 U10 50/70 SPT 25*/70	20.00	4.80	150 blows 25/50						
Remarks								Scale (approx)	Logged By	
								1:50	JE/AK	
								Figure No. SH1085.BH16		

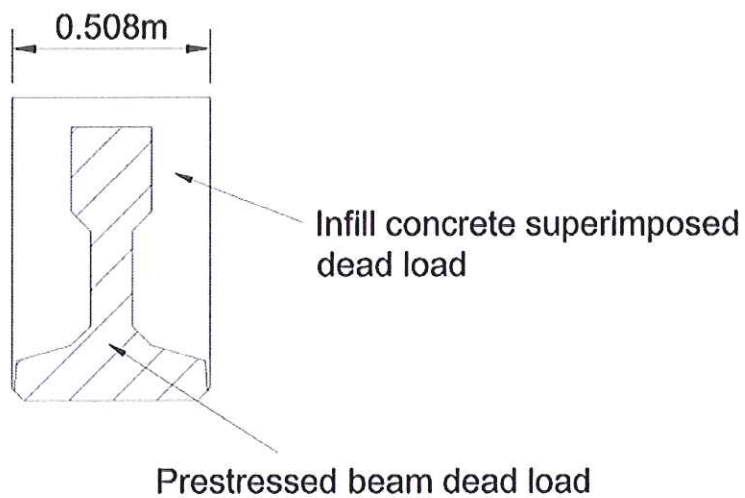
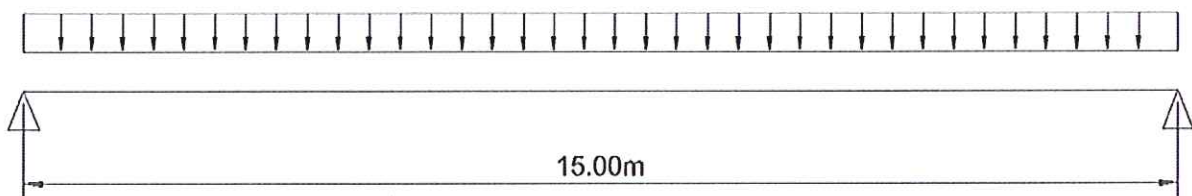


MAY GURNEY						Site Bexhill to Hastings Link Road			Borehole Number BH16	
Boring Method Cable Percussion		Casing Diameter 150mm cased to 7.00m		Ground Level (mOD) 6.72		Client East Sussex County Council			Job Number SI1085	
		Location 576201.473 E 110629.515 N		Dates 08/03/2006-09/03/2006		Engineer Owen Williams			Sheet 3/3	
Depth (m)	Sample / Tests	Casing Depth (m)	Water Depth (m)	Field Records	Level (mOD)	Depth (m) (Thickness)	Description	Legend	Water	Instr
20.00-20.15	D21				-13.43	(2.15) 20.15	Complete at 20.15m	xxxxxx		
Remarks								Scale (approx) 1:50	Logged By JE/AK	Figure No. SI1085.BH16

Appendix D Idealised Structure

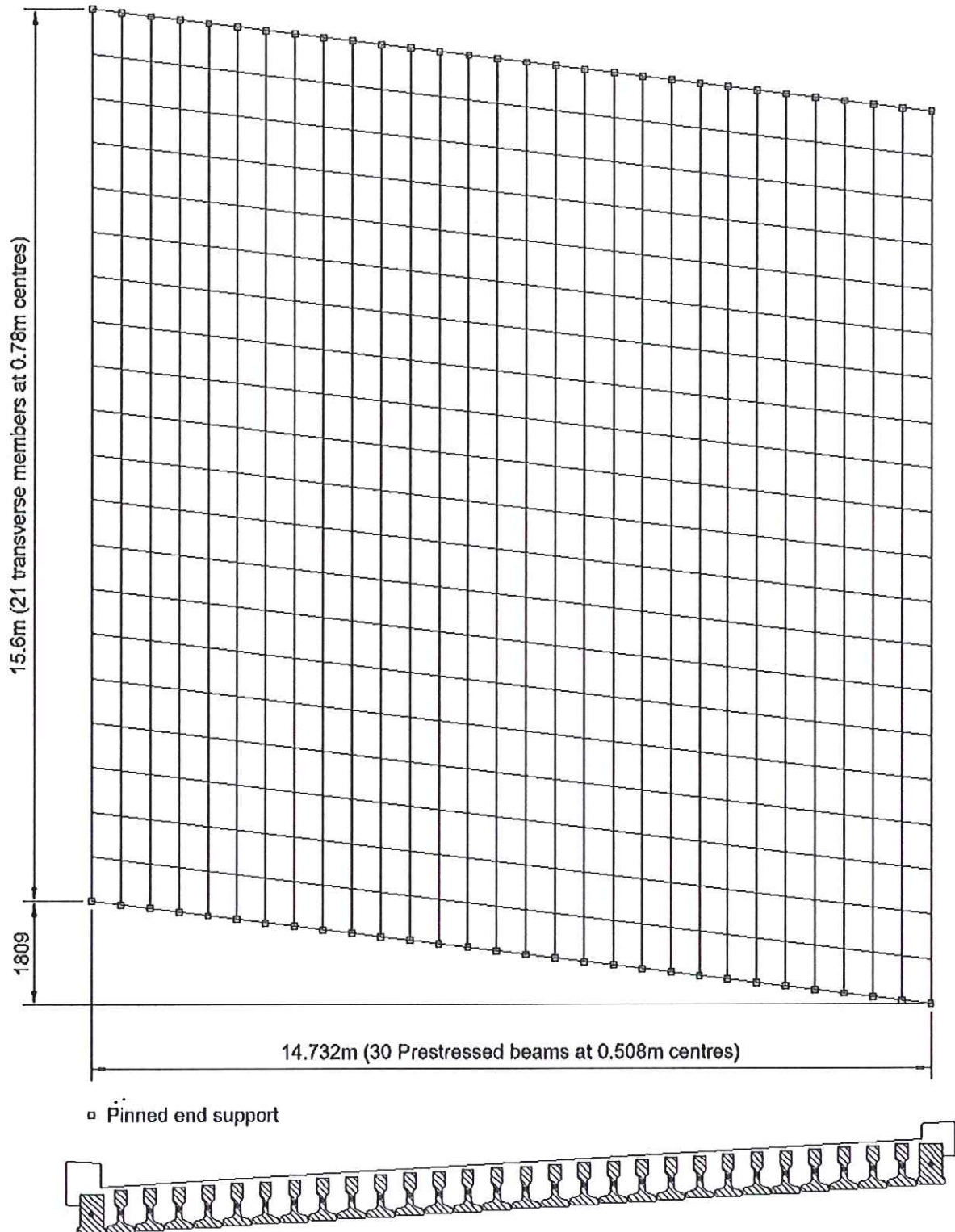
Step 1 Simply supported line beam analysis

- Determine dead and superimposed dead bending moment and shear force distributions.
- 0.508m width beam



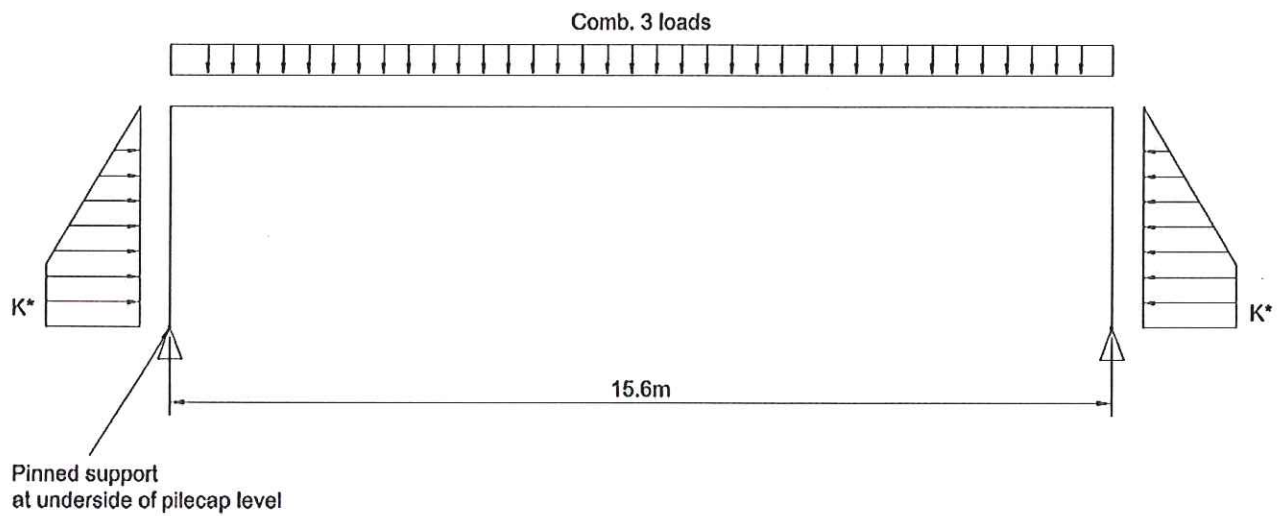
Step 2: Grillage analysis of deck

- Determine live loading combinations 1 and 3 maximum sagging moment
- Determine live loading combinations 1 and 3 shear force distributions
- Determine vertical deck design load for piles



Step 3: Soil structure interaction analysis

- 0.508m width of deck
- Apply combination 3 live loads to deck and passive earth pressures to abutments
- Determine hogging moments at beam ends
- Determine bending moments for pile design
- Determine bending moment and shear force distribution in abutment stem walls



Step 4: Pile design

- Abutment movement and rotation applied to pile heads

